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(54) **Circularly polarized cross dipole antenna**

(57) A circularly polarized cross dipole antenna according to the present invention includes a cross dipole antenna element (A) formed of two pairs of inverted-V-shaped dipole antenna elements (10,30;20,40), which are bent like an inverted "V" at a set angle, so as to cross each other on a ground plane (B), and a feeding mechanism provided to perform a single-point feed through a feeding section (50) common to the inverted-V-shaped dipole antenna elements (10,20,30,40) of the cross dipole antenna element (A).

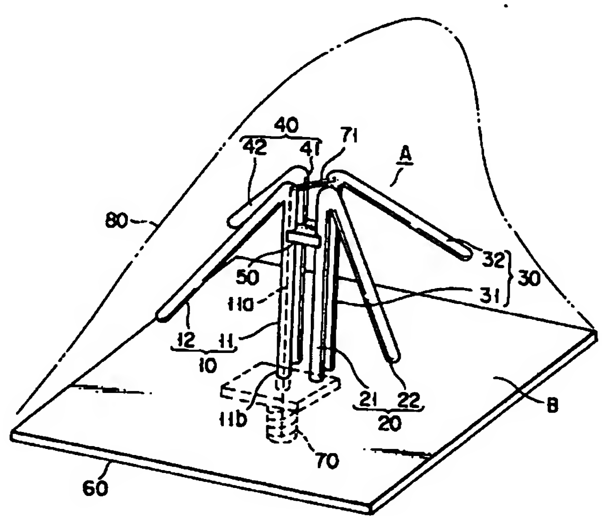

FIG. 1

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Description

[0001] The present invention relates to a circularly polarized cross dipole antenna which is favorably used as a mobile communication antenna for a GPS wave receiving system, a transmitting/receiving system of a satellite communications cellular phone, and the like.

[0002] FIGS. 10A and 10B are illustrations for describing an overview of a prior art circularly polarized cross dipole antenna. FIG. 10A illustrates a dipole antenna, while FIG. 10B does a cross dipole antenna. The dipole antenna shown in FIG. 10A is assembled by forming a single dipole antenna element 101 on a ground plate 100, whereas the cross dipole antenna shown in FIG. 10B is assembled by forming a pair of dipole antennas 101 and 102 on the ground plate 100 so as to cross each other. The cross dipole antenna excites a circularly polarized wave by shifting its phase 90 degrees.

[0003] An axial ratio characteristic is important to an antenna for exciting a circularly polarized wave. In the cross dipole antenna illustrated in FIG. 10B, the axial ratio characteristic of each of the dipole antenna elements 101 and 102 crossing each other is a problem. The axial ratio characteristic becomes good when a gain characteristic of E plane (where an electric field is generated) in each of the dipole antenna elements 101 and 102 is equal to that of H plane (where a magnetic field is generated) therein. When these gain characteristics differ from each other, the axial ratio characteristic becomes worse by an amount corresponding to the difference.

[0004] FIG. 11 is a chart of the comparison of a gain characteristic of E plane (C1 indicated by the solid line) and that of H plane (C2 indicated by the broken line) in the single dipole antenna element 101 shown in FIG. 10A. It is seen from FIG. 11 that the gain characteristics C1 and C2 are different very widely.

[0005] If a cross dipole antenna is assembled by simply crossing two dipole antenna elements having the above characteristics, an axial ratio of them is satisfactory in the vicinity of 0° but it is unsatisfactory at the other angles. It is thus difficult to obtain a circularly polarized cross dipole antenna having a wide-angle axial ratio characteristic even though it is assembled by simply combining two dipole antenna elements having a conventional structure.

[0006] An object of the present invention is to provide a circularly polarized cross dipole antenna having an excellent axial ratio characteristic across a wide angle though its structure is simple.

[0007] To attain the above object, the circularly polarized cross dipole antenna according to the present invention has the following features in structure. The other features of the present invention will be clarified later in the Description of the Invention.

[0008] The circularly polarized cross dipole antenna according to the present invention comprises a cross dipole antenna element formed of two pairs of inverted-V-shaped dipole antenna elements, which are bent like an inverted "V" at a set angle, so as to cross each other on a ground plane; and a feeding mechanism provided to perform a single-point feed through a feeding section common to the inverted-V-shaped dipole antenna elements of the cross dipole antenna element.

[0009] This summary of the invention does not necessarily describe all necessary features so that the invention may also be a sub-combination of these described features.

[0010] The invention can be more fully understood from the following detailed description when taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a perspective view showing a circularly polarized cross dipole antenna according to a first embodiment of the present invention;
FIG. 2 is a top view of the circularly polarized cross dipole antenna according to the first embodiment of the present invention;
FIG. 3 is a side view of the circularly polarized cross dipole antenna according to the first embodiment of the present invention;
FIG. 4 is a chart for describing a function of an inverted-V-shaped dipole antenna element of the circularly polarized cross dipole antenna according to the first embodiment of the present invention;
FIG. 5 is a graph showing conditions for acquiring a wide-angle axial ratio characteristic of the circularly polarized cross dipole antenna according to the first embodiment of the present invention;
FIG. 6 is a graph showing the optimum-structure data acquired when an inclination angle of the circularly polarized cross dipole antenna according to the first embodiment of the present invention is varied;
FIG. 7 is a graph showing a relationship between the 3dB width (half-value angle) of axial ratio and gain and the input impedance with respect to the inclination angle when the circularly polarized cross dipole antenna according to the first embodiment of the present invention has the optimum structure;
FIG. 8 is a chart showing a typical example of the axial ratio characteristic and the gain characteristic of the circularly polarized cross dipole antenna according to the first embodiment of the present invention;
FIG. 9 is a partly cutaway side view of the main part of a circularly polarized cross dipole antenna according to a second embodiment of the present invention;
FIGS. 10A and 10B are illustrations for describing an overview of a prior art circularly cross dipole antenna; and
FIG. 11 is a chart of the comparison of a gain characteristic of E plane and that of H plane in the prior

art circularly polarized cross dipole antenna.

(First Embodiment)

[0011] As illustrated in FIGS. 1 to 3, a circularly polarized cross dipole antenna according to the first embodiment includes a cross dipole antenna element A constituted of four inverted-V-shaped dipole antenna elements 10, 20, 30 and 40 which are integrated as one unit. The dipole antenna elements 10, 20, 30 and 40 include their respective pole portions 11, 21, 31 and 41, and the pole portions 11, 21, 31 and 41 have their respective arm portions 12, 22, 32 and 42 at their tops. The "inverted-V-shaped" means that the arm portions 12, 22, 32 and 42 are each inclined from the top toward the ground at a given angle θs.

[0012] Focusing attention to one dipole antenna element 10, it includes a pole portion 11 standing vertically on a ground plane B (the surface of ground member 60) and having a height H and an arm portion 12 one end of which is coupled to the top of the pole portion 11 and the other end of which is held in a position where it is closer to the ground plane B than the one end of the arm portion 12. The arm portion 12 is thus inclined at the given angle θs.

[0013] The other elements 20, 30 and 40 also include pole portions 21, 31 and 41 and arm portions 22, 32 and 42, respectively.

[0014] The pole portions 11, 21, 31 and 41 of the dipole antenna elements 10, 20, 30 and 40 are coupled to one another by means of a short-circuit member 50 at a distance of Hs from their tops. The pole portions 11, 21, 31 and 41 are therefore electrically short-circuited at the coupling portion to achieve a single-point feed structure. In other words, the dipole antenna elements 10, 20, 30 and 40 are so designed as to perform a single-point feed through the short-circuit member 50 which is a common feeding section of a feeding mechanism F.

[0015] As illustrated in FIG. 1, one of the pole portions 11, 21, 31 and 41 of the dipole antenna elements 10, 20, 30 and 40, e.g., the pole portion 11 is so constituted that its core wire 11a and conductive pipe 11b are arranged coaxially with each other. The proximal end of the conductive pipe 11b is connected to the ground member 60, while that of the core wire 11a insulatively penetrates the ground member 60 and then connects to the central conductor of a coaxial feeder-connecting connector 70 attached to the underside of the ground member 60.

[0016] The distal end of the core wire 11a is connected to that of the conductive pipe 11b at the top of the pole portion 11. The top of the pole portion 11 is short-circuited with that of another pole portion 31, which stands diagonally with respect to the pole portion 11, by means of a conductor 71.

[0017] In order to mount the above-described antenna on an object such as an automobile, it is preferable that the ground member 60 be used as a mount plate and the entire antenna be covered with a cover 80 having a streamlined shape or another desired shape.

[0018] If, as described above, the dipole antenna elements 10, 20, 30 and 40 are each shaped like an inverted "V", the gain characteristics of E and H planes in each of the antenna elements are approximate to each other across a wide angle. This situation is specifically shown in FIG. 4.

[0019] In FIG. 4, characteristic curve C11 indicates the gain characteristic of E plane when the inclination angle θs is 0°, character curve C12 indicates the gain characteristic of H plane when the inclination angle θs is 0°, character curve C13 indicates the gain characteristic of E plane when the inclination angle θs is 45°, and character curve C14 indicates the gain characteristic of H plane when the inclination angle θs is 45°.

[0020] It is apparent from FIG. 4 that the gain characteristics of E and H planes are different from each other so widely when the angle θs is 0°. In contrast, they are considerably closer to each other when the angle θs is 45°.

[0021] If, therefore, the four inverted-V-shaped dipole antenna elements 10, 20, 30 and 40 are combined by properly setting the inclination angle θs, the circularly polarized cross dipole antenna having an axial ratio characteristic can be obtained as shown in FIG. 1.

[0022] A condition for acquiring an excellent axial ratio characteristic across a wide angle will now be described. If the gain characteristics of E and H planes of the dipole antenna elements 10, 20, 30 and 40 are set equal to each other, the axial ratio characteristic is satisfied. By varying the height H of each of the pole portions 11, 21, 31 and 41 of the dipole antenna elements 10, 20, 30 and 40, the length L of each of the arm portions 12, 22, 32 and 42, and the inclination angle θs, the length L was obtained by simulation such that a difference between the gain characteristics of E and H planes in the range from 0° to 60° was minimized.

[0023] If the real part R and imaginary part X of input impedance Z does not satisfy the following relationship: $R = -X$, a difference between gains of E and H planes at an inclination angle of 0° does not become zero and thus no polarized waves are obtained. The structure for satisfying the above condition was also obtained by simulation.

[0024] FIG. 5 is a graph showing results of the above simulation. In FIG. 5, the horizontal axis represents the inclination angle θs and the vertical axis does the length L of each of the arm portions 12, 22, 32 and 42 on a wavelength basis. C21 to C25 indicate a relationship between the inclination angle θs and the length L of each of the arm portions 12, 22, 32 and 42 when the above height H is used as a parameter. Further, C20 indicates a relationship between the inclination angle θs and the length L of each of the arm portions 12, 22, 32 and 42 to satisfy the second condition: $R = -X$ for obtaining a circularly polarized wave.

[0025] If both the condition of $R = -X$ in the imped-

ance X and that of the length L of each of the arm portions 12, 22, 32 and 42 corresponding to variations in the height H of the pole portions 11, 12, 31 and 41 are satisfied simultaneously, an excellent axial ratio characteristic can be obtained. In FIG. 5, therefore, intersection points of the curves C21 to C25 and the curve C20 correspond to the conditions for obtaining the excellent axial ratio characteristic.

[0026] Next a distance Hs from the top of each of the pole portions 11, 21, 31 and 41 to the short-circuit member 50 will be described. When the cross dipole antenna has a single-point feed structure, the axial ratio characteristics greatly depends upon how the height of the short-circuit member 50 for short-circuiting the pole portions 11, 21, 31 and 41, i.e., the distance Hs is determined. The input impedance Z(X/R) of the dipole antenna, the height H of the pole portions 11, 21, 31 and 41, the height of the short-circuit member 50, i.e., the distance Hs are expressed by the following equation:

$$X/R = \sin\beta(H + Hs)/\sin\beta(H - Hs) \qquad (1)$$

where β is a phase constant.

[0027] Hereinafter the above equation will be called an Hs design equation (1). By setting the distance Hs based on the equation (1), a good axial ratio characteristic can be secured.

[0028] The structure of the cross dipole antenna having good axial ratio characteristic will now be described.

[0029] As described above referring to FIG. 5, the height H of each of the pole portions 11, 21, 31 and 41 and the length L of each of the arm portions 12, 22, 32 and 42 corresponding to the height H can be measured by the inclination angle θs. The cross dipole antenna having a single-point feed structure can be optimized from the input impedance Z and the Hs design equation (1).

[0030] FIG. 6 is a graph showing the optimum-structure data of the cross dipole antenna which is acquired when the inclination angle θs is varied, that is, the optimum interrelationship among the height H of each of the pole portions 11, 21, 31 and 41, the length L of each of the arm portions 12, 22, 32 and 42, and the distance Hs from the top of each of the pole portions to the short-circuit member 50 with respect to the inclination angle θs.

[0031] FIG. 7 is a graph showing a relationship between the 3dB width (half-value angle) of axial ratio and gain and the input impedance with respect to the inclination angle θs when the cross dipole antenna has the optimum structure.

[0032] FIG. 8 is a chart showing the gain and axial ratio characteristics when the inclination angle θs is varied from 0° to 45° and from 45° to 80°. Unless a distance d between opposing pole portions is sufficiently small, an error of the Hs design equation (1) is increased. For this reason, d is set equal to 10^{-4} λ. When the inclination angle θs of each of the arm portions 12, 22, 32 and 42 is set to approximately 5° as shown in FIG. 8, the 3dB width of the axial ratio is considerably increased.

[0033] It is thus seen from FIG. 8 that the distance Hs from the top of each of the pole portions 11, 21, 31 and 41 to the short-circuit member 50 is uniquely determined for the inclination angle θs and, if the inclination angle θs is determined without being set to an extreme value, the length L of each of the arm portions and the distance Hs produce an excellent axial ratio characteristic.

[0034] The circularly polarized cross dipole antenna according to the first embodiment of the present invention has a single-point feed structure in which the dipole antenna elements 10, 20, 30 and 40 are bent and shaped like an inverted "V" and the pole portions 11, 21, 31 and 41 are employed. A circularly polarized dipole antenna having a simple feed structure and a wide-angle axial ratio characteristic can thus be attained. The structure of the antenna can be achieved easily and accurately by setting the height H of each of the pole portions 11, 21, 31 and 41, the length L of each of the arm portions 12, 22, 32 and 42, the inclination angle θs of each of the arm portions 12, 22, 32 and 42, the height Hs of the short-circuit member 50, and impendence Z, so as to approximate the gain characteristics of E and H planes of each of the dipole antenna elements 10, 20, 30 and 40 to each other. Consequently, a circularly polarized cross dipole antenna for fulfilling a desired function can stably be provided.

(Second Embodiment)

[0035] FIG. 9 is a side view showing a major part of a circularly polarized cross dipole antenna according to a second embodiment of the present invention. It is in an angle adjustment mechanism 93 for variably setting the inclination angle θs of an arm portion 92 that the second embodiment differs from the first embodiment. More specifically, one end of the arm portion 92 is coupled to the top of a pole portion 91 such that it can be moved up and down, as indicated by double-headed arrow y in FIG. 9, by means of a shaft mechanism 94. In order to stabilize the adjusted inclination angle θs, the arm portion 92 can be supported by an insulating support member 95 which is slidably fitted on the pole portion 91 as indicated by double-headed arrow z. Thus, the inclination angle of the arm portion 92 can be set variably.

(Features of the Embodiments)

[0036]

[1] A circularly polarized cross dipole antenna according to the embodiments, wherein paired

dipole antenna elements (10, 30; 20, 40) are each bent like an inverted "V" to control a gain characteristic of the antenna and an axial ratio characteristic thereof.

[2] A circularly polarized cross dipole antenna according to the embodiments, which allows a circularly polarized wave to be excited by arranging paired dipole antenna elements (10, 30; 20, 40) so as to cross each other, wherein the paired dipole antenna elements (10, 30; 20, 40) are inverted-V-shaped antenna elements each of which is bent like an inverted "V" at a set angle.

[3] The circularly polarized cross dipole antenna described in above item [2], wherein the inverted-V-shaped antenna elements have pole portions (11, 21, 31, 41) standing vertically on a ground plane (B) and arm portions (12, 22, 32, 42) inclined at a set inclination angle (θs) such that one end of each of the arm portions is coupled to a top of each of the pole portions and another end thereof is held in a position closer to the ground plane (B) than the one end of each of the arm portions.

[4] The circularly polarized cross dipole antenna described in above item [3], wherein the pole portions (11, 21, 31, 41) of the inverted-V-shaped antenna elements are coupled to one another by a short-circuit member (50) to have a single-point feed structure.

[5] The circularly polarized cross dipole antenna described in above item [3], comprising an angle adjustment mechanism (93) for variably setting the inclination angle (θs) of an arm portion (92).

(Modifications)

[0037] The circularly polarized cross dipole antenna described in the above embodiments includes the following modifications:

i) A dipole antenna element having a gently-curved or acute-angled L-shaped arm portion; and

ii) A dipole antenna element formed by adhering a thin-film conductor onto a substrate.

Claims

1. A circularly polarized cross dipole antenna characterized by comprising:

   a cross dipole antenna element (A) formed of two pairs of inverted-V-shaped dipole antenna elements (10, 30; 20, 40), which are bent like an inverted "V" at a set angle (θs), so as to cross each other on a ground plane (B); and

   a feeding mechanism (F) provided to perform a single-point feed through a feeding section (50) common to the inverted-V-shaped dipole antenna elements (10, 20, 30, 40) of the cross dipole antenna element (A).

2. The circularly polarized cross dipole antenna according to claim 1, characterized in that each of the inverted-V-shaped dipole antenna elements (10, 20, 30, 40) has a pole portion (11, 21, 31, 41) standing vertically on the ground plane (B) and an arm portion (12, 22, 32, 42) inclined at an inclination angle (θs) such that one end of each of the arm portions (12, 22, 32, 42) is coupled to a top of each of the pole portions (11, 21, 31, 41) and another end thereof is held in a position closer to the ground plane (B) than the one end of each of the arm portions (12, 22, 32, 42).

3. The circularly polarized cross dipole antenna according to claim 2, characterized by further comprising an angle adjustment mechanism (93) for variably setting the inclination angle (θs) of the arm portion (92).

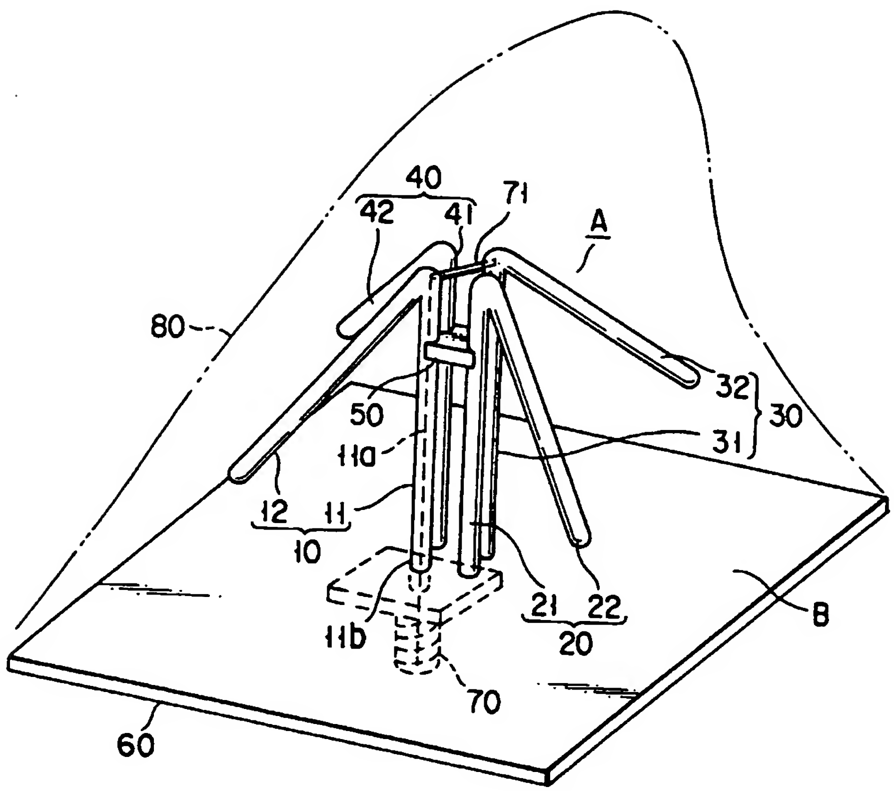


FIG. 1

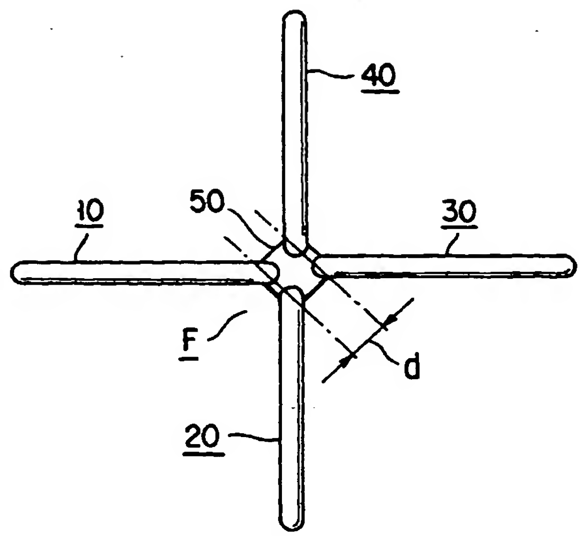


FIG. 2

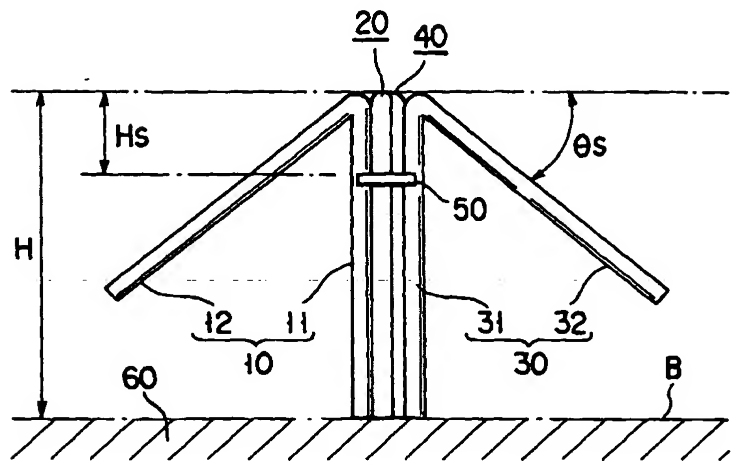


FIG. 3

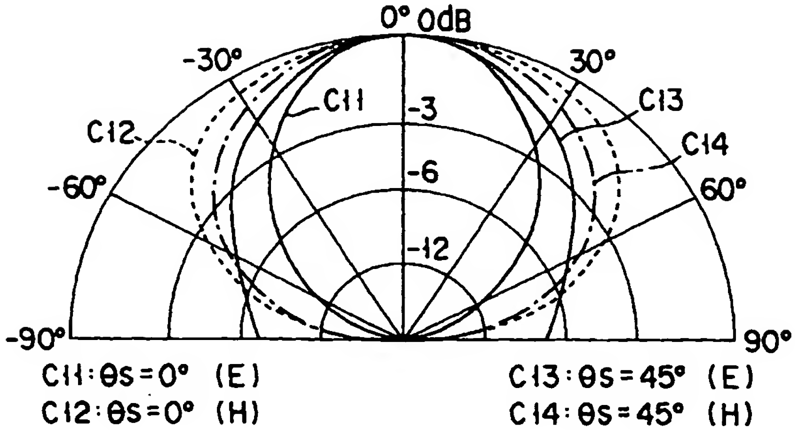

0° 0dB
-30°
30°
C11
-3
C12
C13
C14
-6
-60°
60°
-12
-90°
90°
C11:θs=0° (E)
C12:θs=0° (H)
C13:θs=45° (E)
C14:θs=45° (H)

FIG. 4

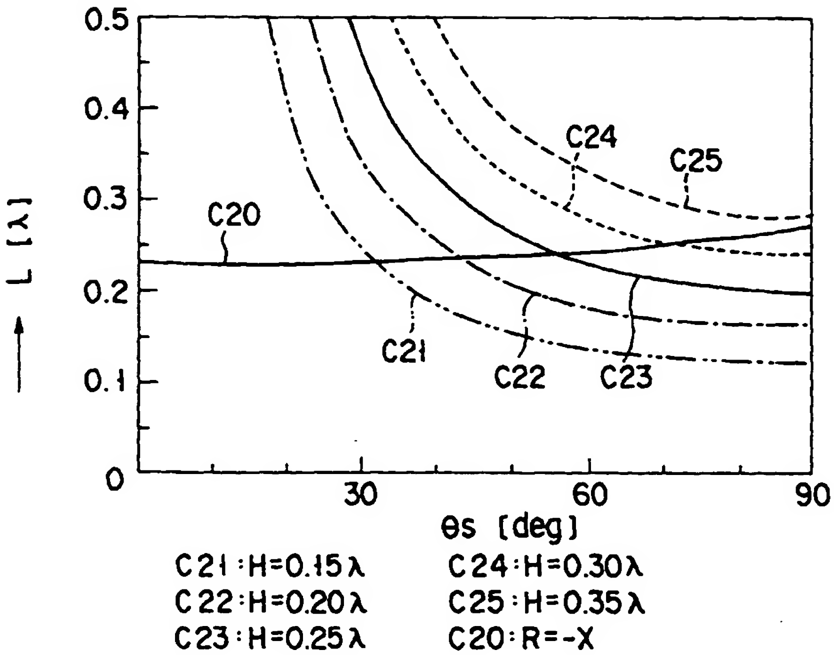

0.5
0.4
0.3
0.2
0.1
0
L [λ]
C20
C21
C22
C23
C24
C25
30
60
90
θs [deg]
C21:H=0.15λ
C22:H=0.20λ
C23:H=0.25λ
C24:H=0.30λ
C25:H=0.35λ
C20:R=-X

FIG. 5

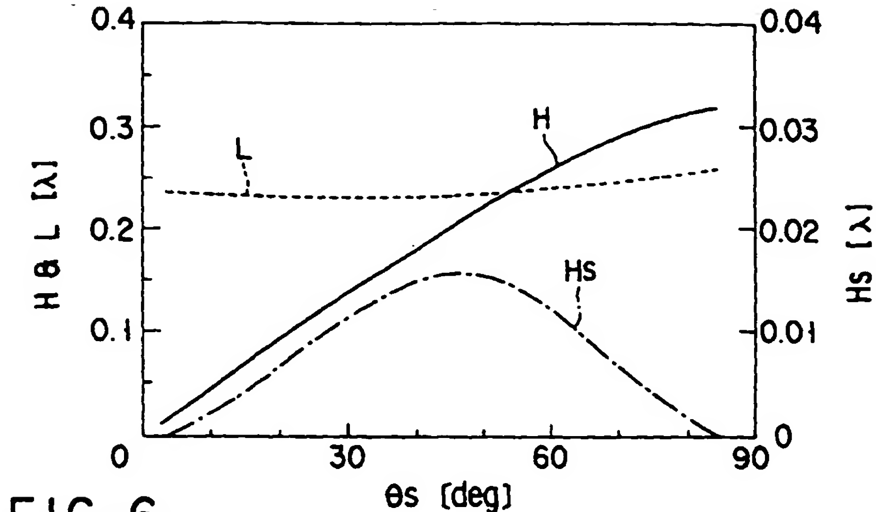
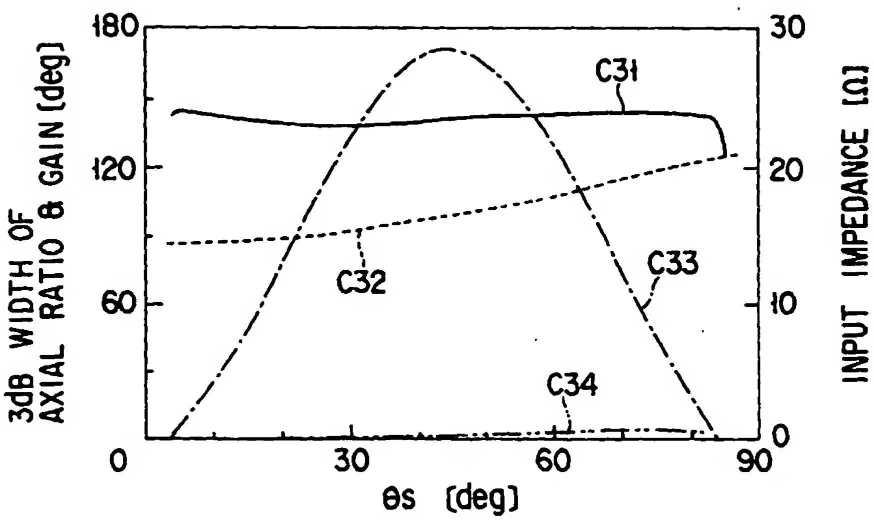


FIG. 6



C31: 3dB WIDTH OF AXIAL RATIO
C32: 3dB WIDTH OF GAIN
C33: IMPEDANCE (REAL)
C34: IMPEDANCE (IMAGINARY)

FIG. 7

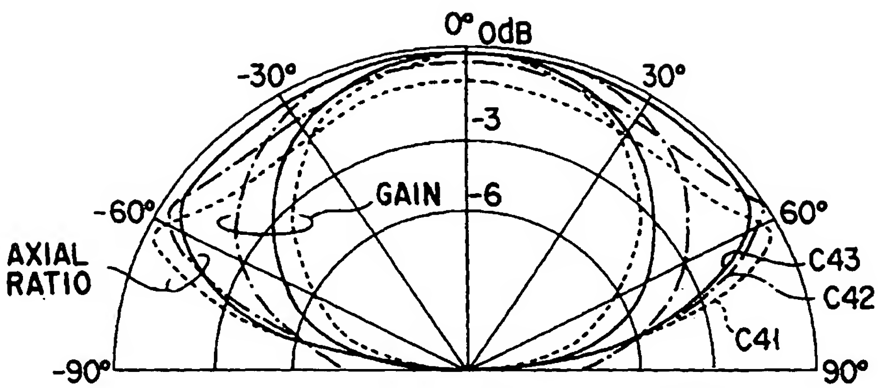


FIG. 8

C41: θs = 5° (7.87dBi)
C42: θs = 45° (6.82dBi)
C43: θs = 80° (6.12dBi)

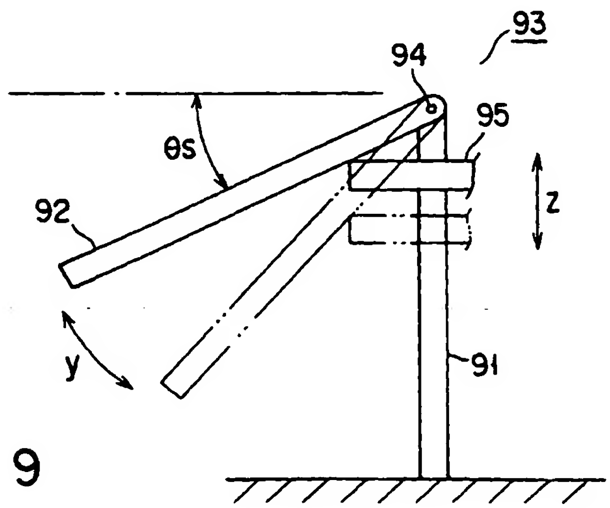


FIG. 9

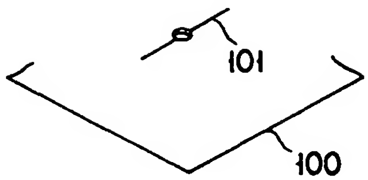


FIG. 10A

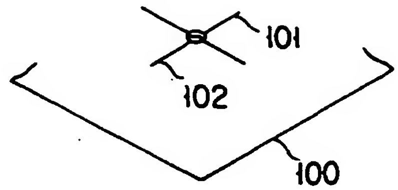


FIG. 10B

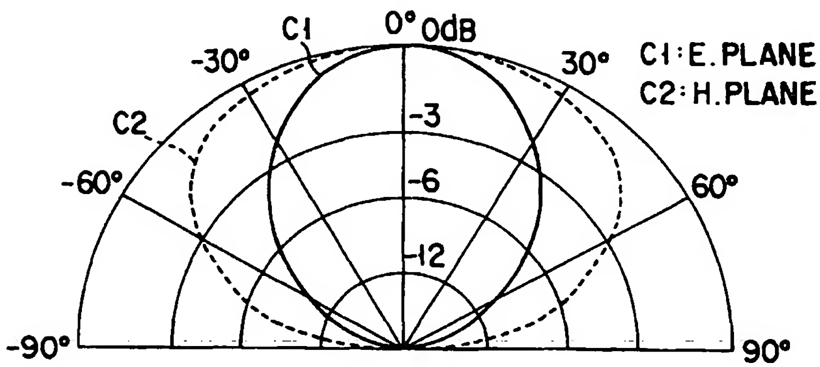


FIG. 11

European Patent Office

EUROPEAN SEARCH REPORT

Application Number
EP 00 30 2874

DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
X Y	US 4 062 019 A (WOODWARD OAKLEY MCDONALD ET AL) 6 December 1977 (1977-12-06) * column 1, line 31 - line 46 * * column 2, line 9 - line 68 * * column 3, line 1 - line 50; claims 1,3,4; figures 1-3 *	1 2	H01Q11/06 H01Q21/26 H01Q21/24
Y	US 4 446 465 A (DONOVAN JOSEPH A) 1 May 1984 (1984-05-01) * column 1, line 49 - line 63 * * column 2, line 41 - line 66 * * column 3, line 1 - line 57; claims 1,2; figures 1-3 *	2	
A	EP 0 936 693 A (SONY INT EUROP GMBH) 18 August 1999 (1999-08-18) * column 5, line 42 - line 49; claims 1,4; figures 4,5 *	3	
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
			H01Q

The present search report has been drawn up for all claims

Place of search	Date of completion of the search	Examiner
THE HAGUE	18 January 2001	Moumen, A

CATEGORY OF CITED DOCUMENTS

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ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO. EP 00 30 2874

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The members are as contained in the European Patent Office EDP file on
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18-01-2001

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4062019 A	06-12-1977	NONE	
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For more details about this annex : see Official Journal of the European Patent Office, No. 12/82